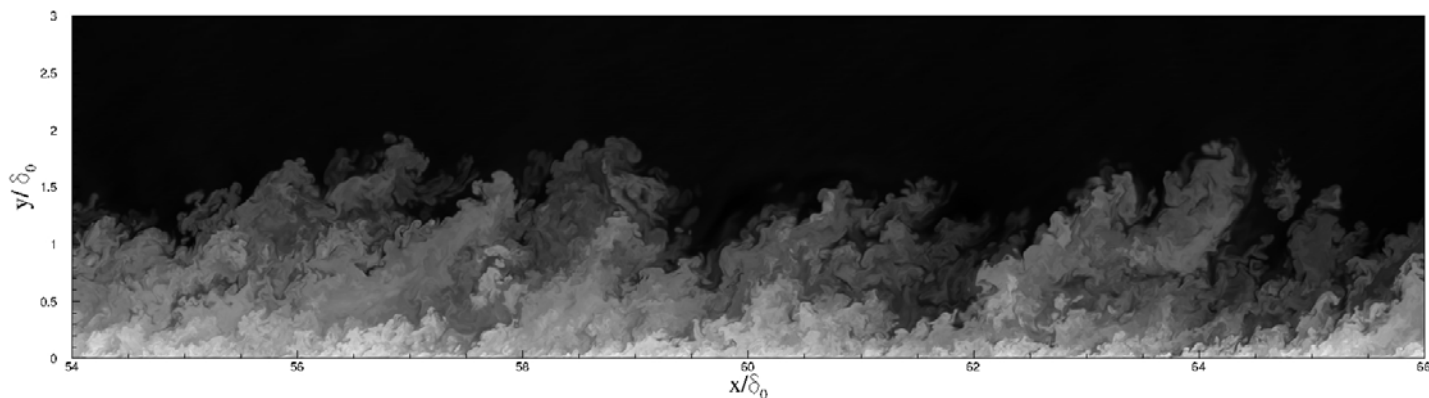


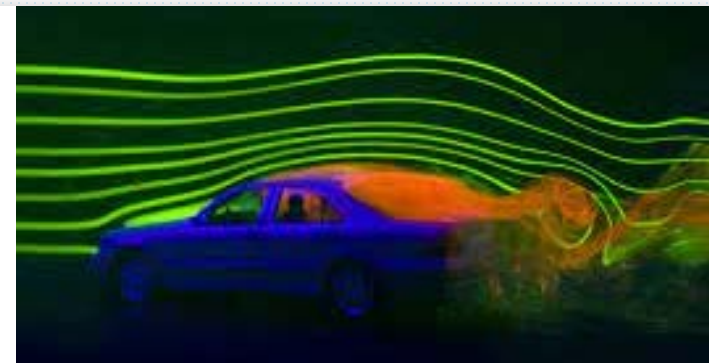


Background

When turbulence meets wall



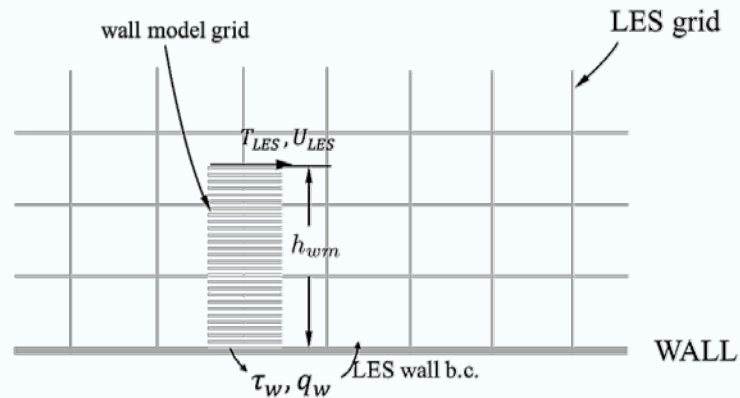
- Tremendous smaller scales at inner layer
- Chapman (1979): $N_{pts} \sim Re_c^{1.8}$ required to resolve inner layer
- DNS resolution: $N_{pts} \sim Re_c^{2.25}$
- Prohibitive computational cost





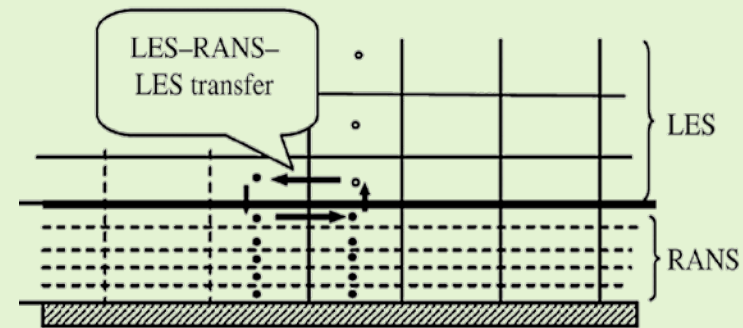
Different wall-modeling techniques

• Wall-Modeled LES



- *LES formulation over the whole domain*
- *Wall shear-stress provided by a wall model and feeding to LES as boundary conditions*
- *Much less model parameters*

• Hybrid RANS/LES



- *LES formulation away from wall*
- *RANS formulation near walls*
- *Interface location shall be carefully selected*
- *Include many parameter in the RANS region*



Physics-based wall-shear-stress model:

- We can view the DG solution as a local modal decomposition

$$U_e(t, x) = \sum_{i=1}^{N_p} \tilde{U}_{e,i}(t) \phi_{e,i}(x), \quad x \in \Omega_e$$

Linear basis

Remaining part
projected to log basis

$$\tau_w/\rho = \nu \frac{\partial u_{//}}{\partial y} \Big|_{y=0}$$

linear mode should dominate
if the BL is resolved up to the
viscous sublayer

log mode should dominate
if the wall-adjacent cell is
situated in log-law region

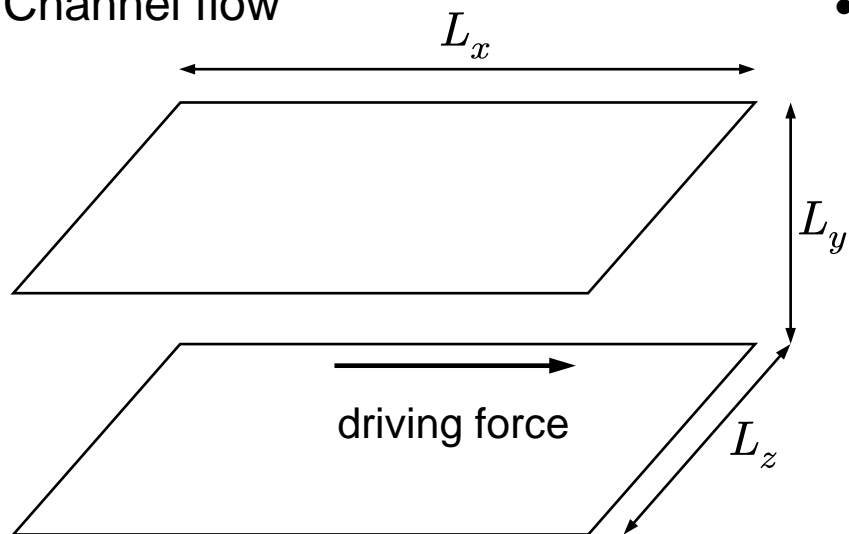
$$u_{//} = \frac{u_\tau}{\kappa} \log\left(\frac{y}{y_0}\right)$$
$$\tau_w/\rho = u_\tau^2$$

- The modeled wall-shear-stress is the sum of both contributions



Validation study

- Channel flow

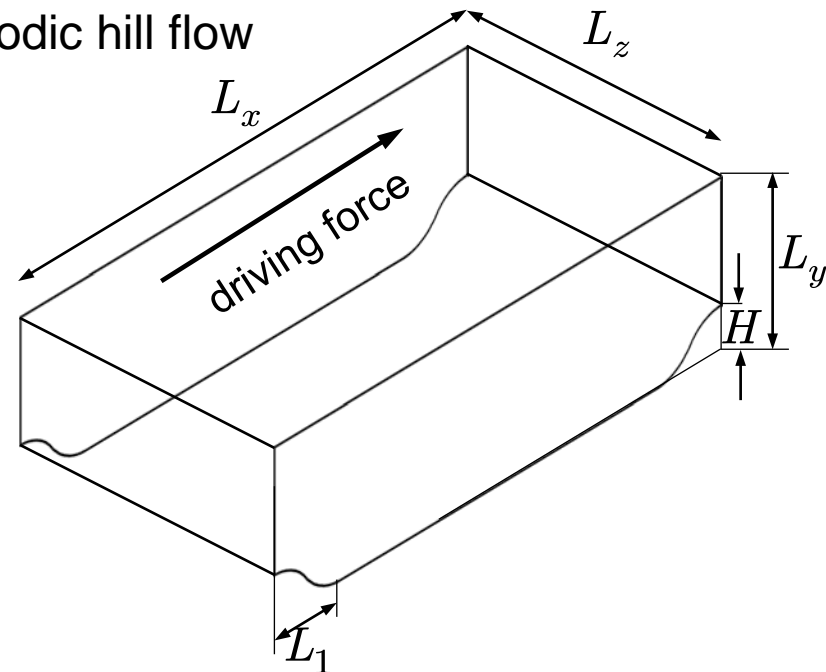


Domain ○ $L_x \times L_y \times L_z \in 2\pi h \times 2h \times 2\pi h$

Mesh size $DoF = n_x \times n_y \times n_z = 32^3, 64^3, 128^3$
(DGP3)

Reynolds No. ○ $Re_\tau = 180, 2000, 50000$

- Periodic hill flow



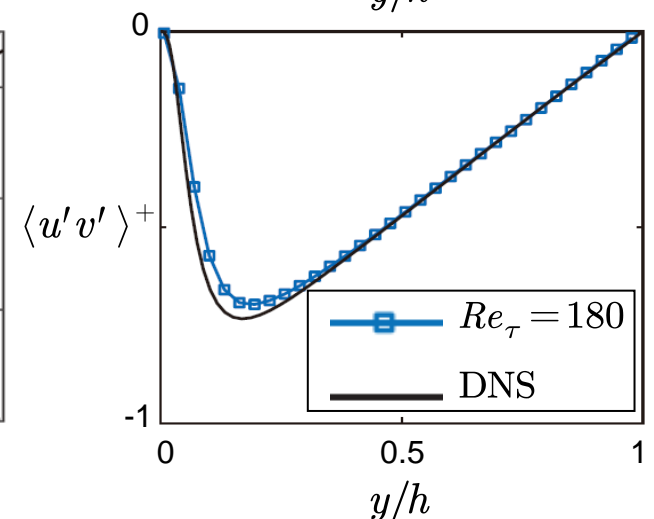
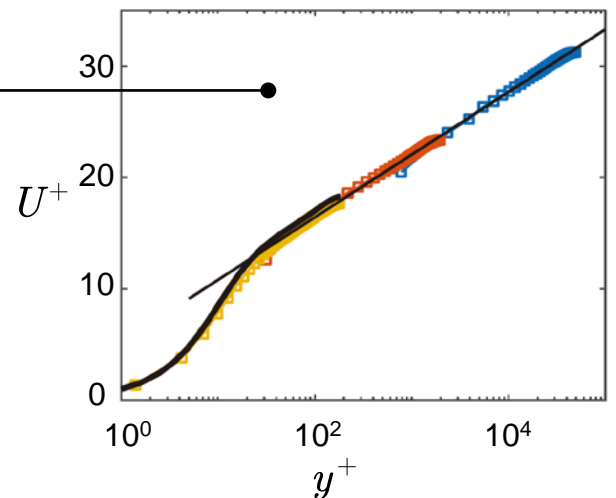
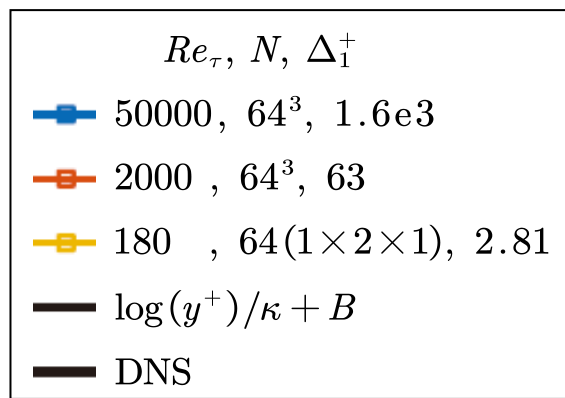
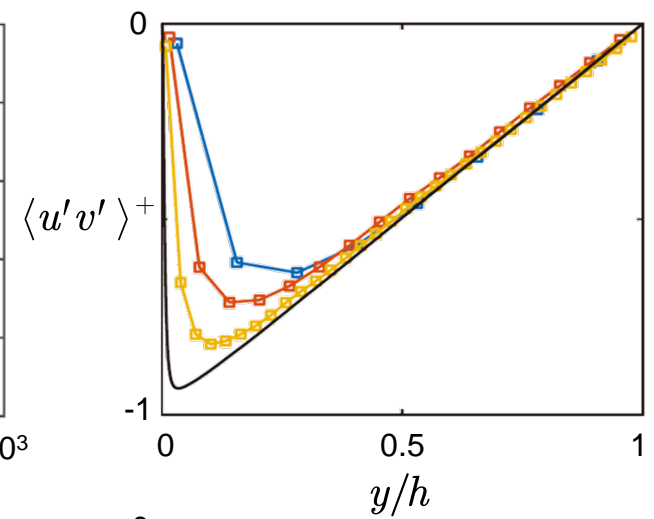
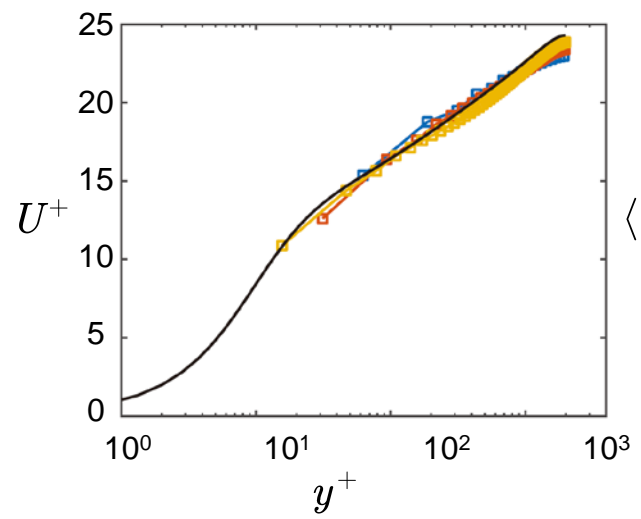
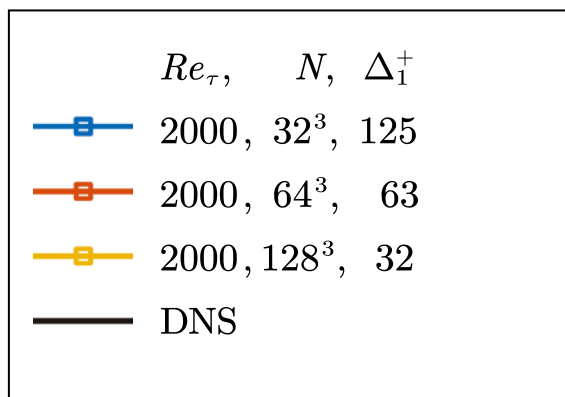
○ $L_x \times L_y \times L_z = 9H \times 3.036H \times 4.5H,$
 $L_1 = 1.929H$

$DoF = n_x \times n_y \times n_z = 32(2 \times 1 \times 1), 64^3$

○ $Re_b = HU_b/\nu = 10595$

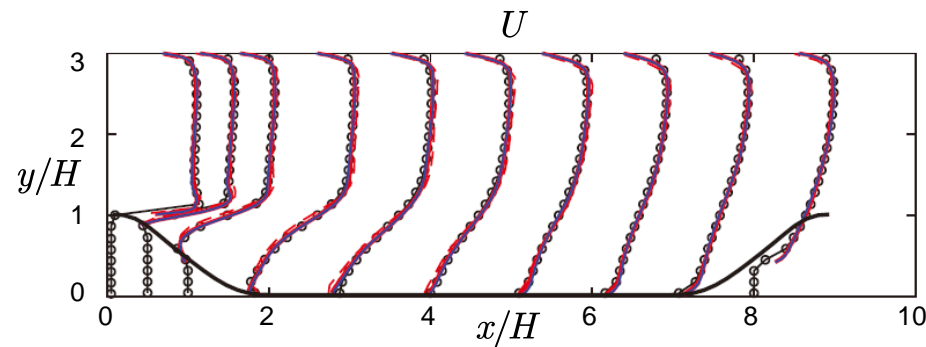


Validation study on WMLES—channel flow

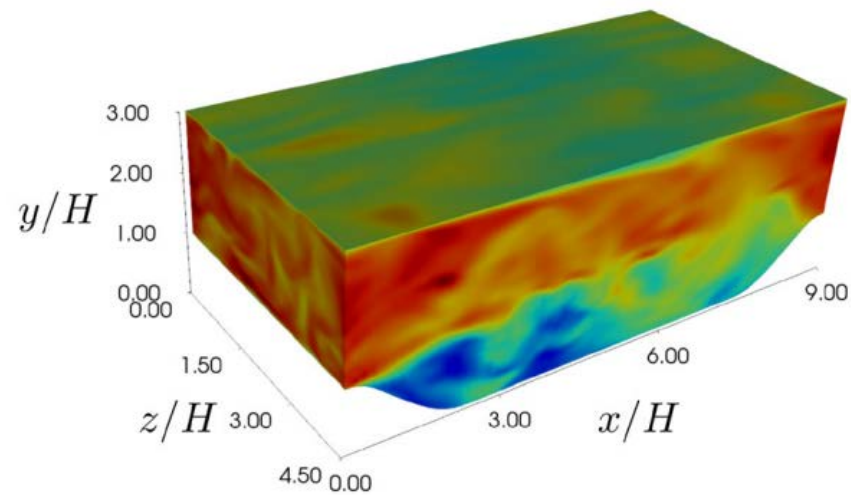
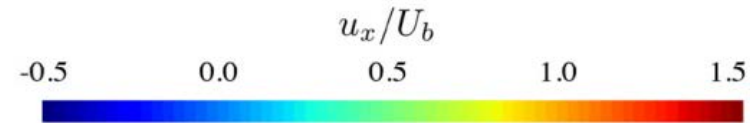
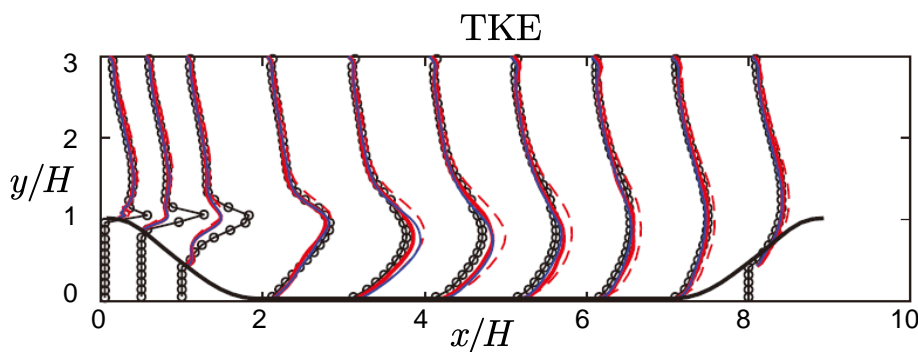
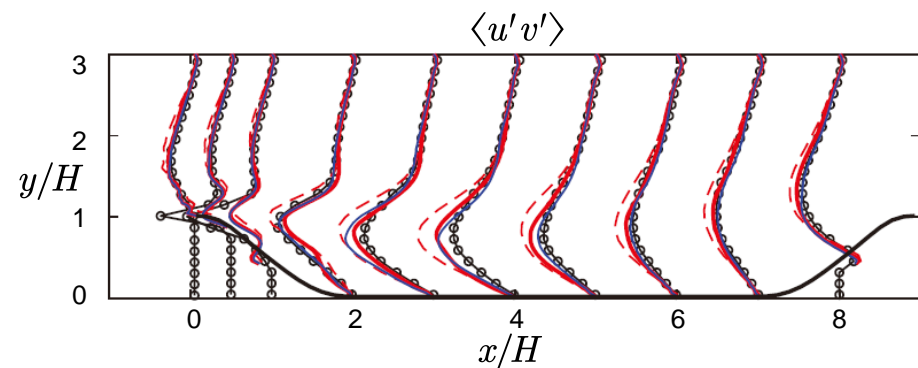




Validation study on WMLES—periodic hill flow



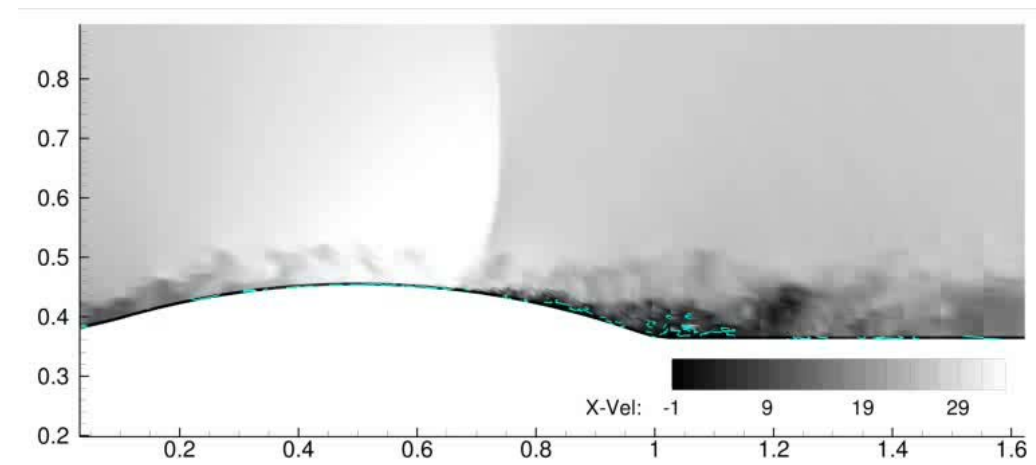
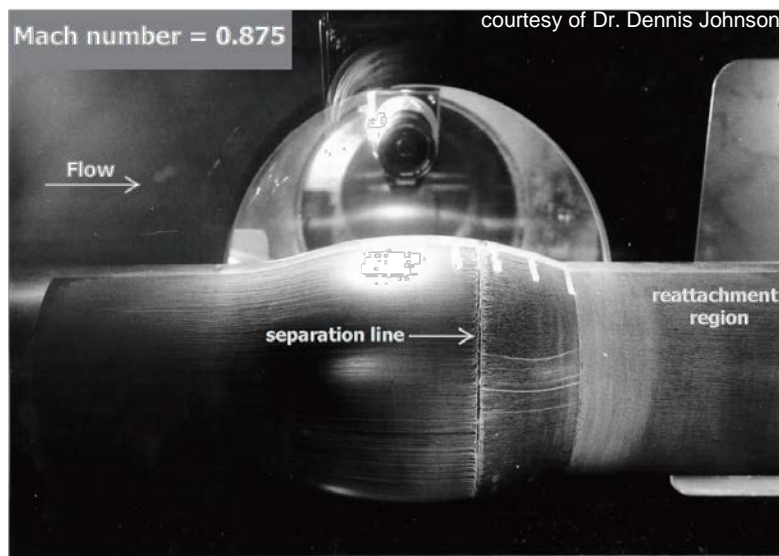
- $DoF = 64^3$
- - - $DoF = 64 \times 32 \times 32$
- *Wall-resolved results*



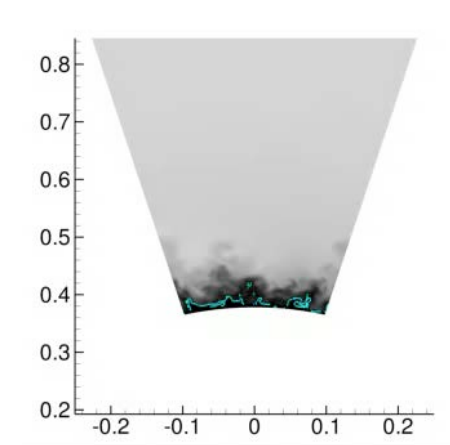


WMLES of NASA transonic bump configuration

- NASA transonic bump configuration



- Key flow features: separation bubble; weak shock
- Computational setup:
 - DGP3; tensor basis; hexahedron
 - 218,000 elements; 64 DoF per element; 14M DoF



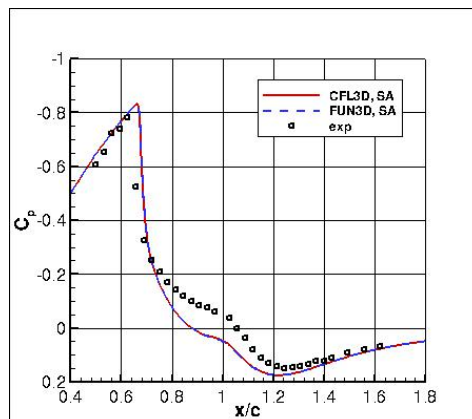


WMLES of NASA transonic bump configuration

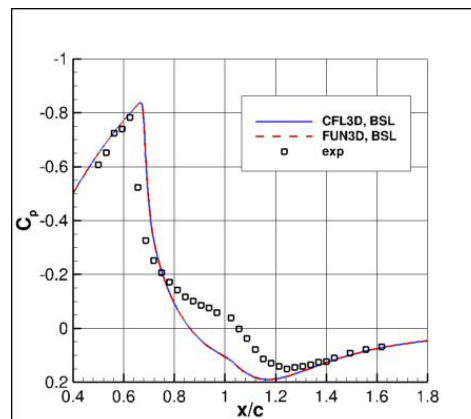
- Existing RANS results

Pressure coefficient

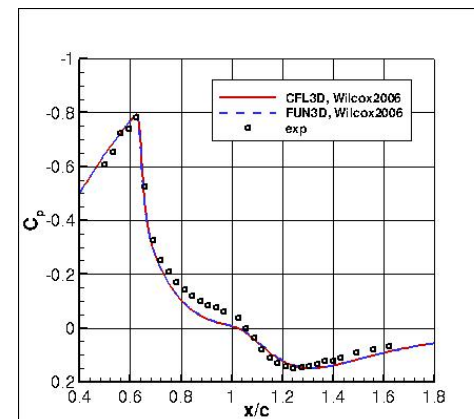
SA model



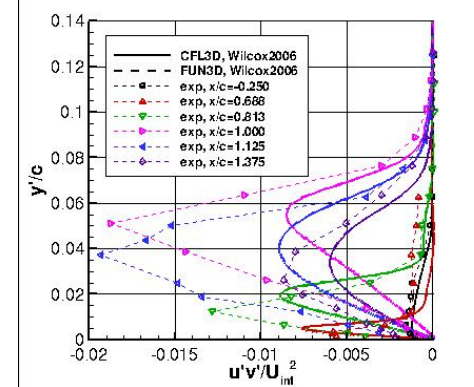
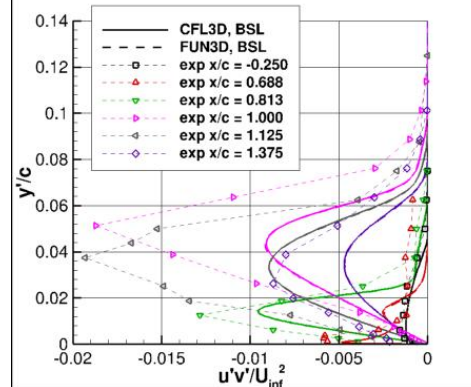
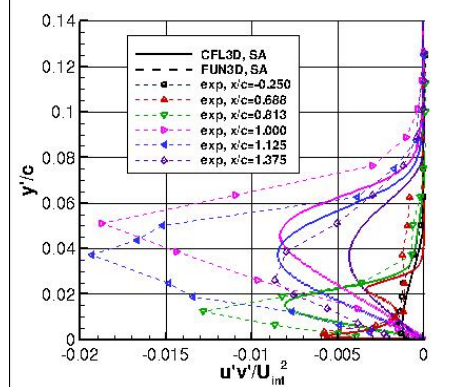
SST model



Wilcox-Kim model



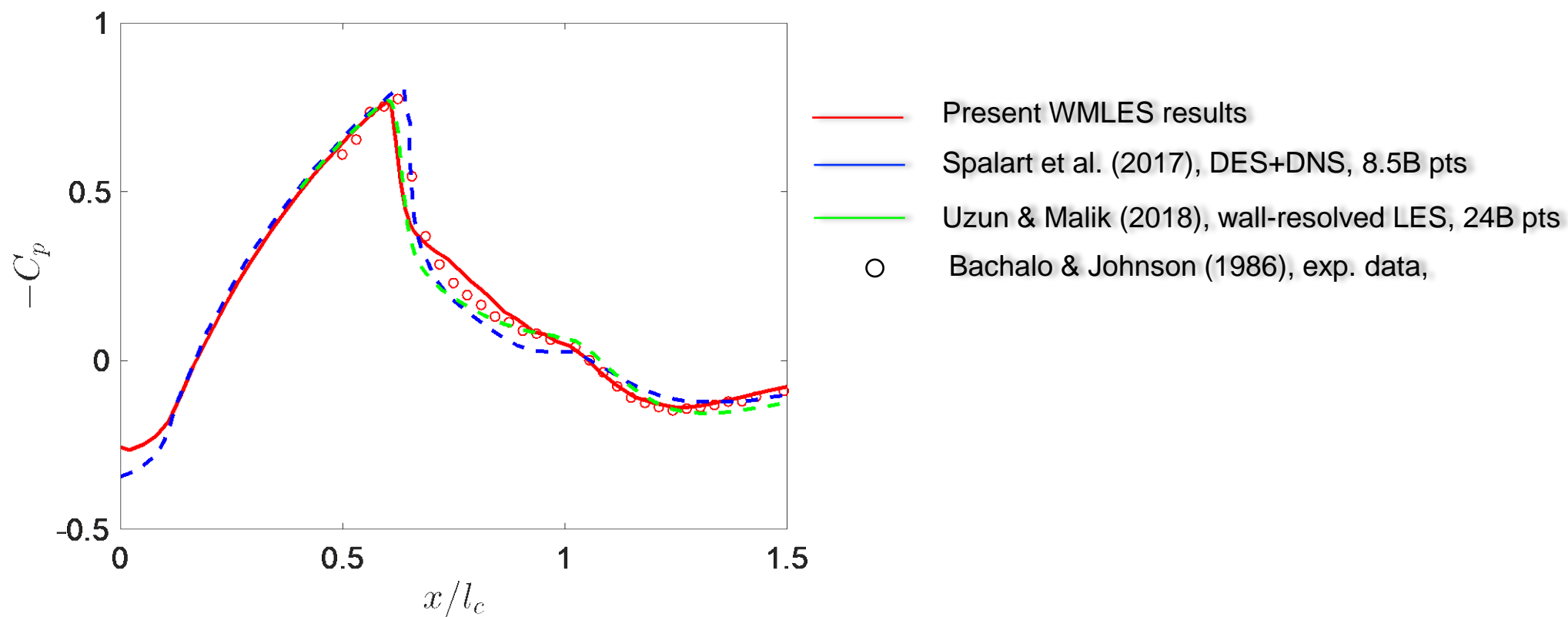
Reynold stress





WMLES of NASA transonic bump configuration

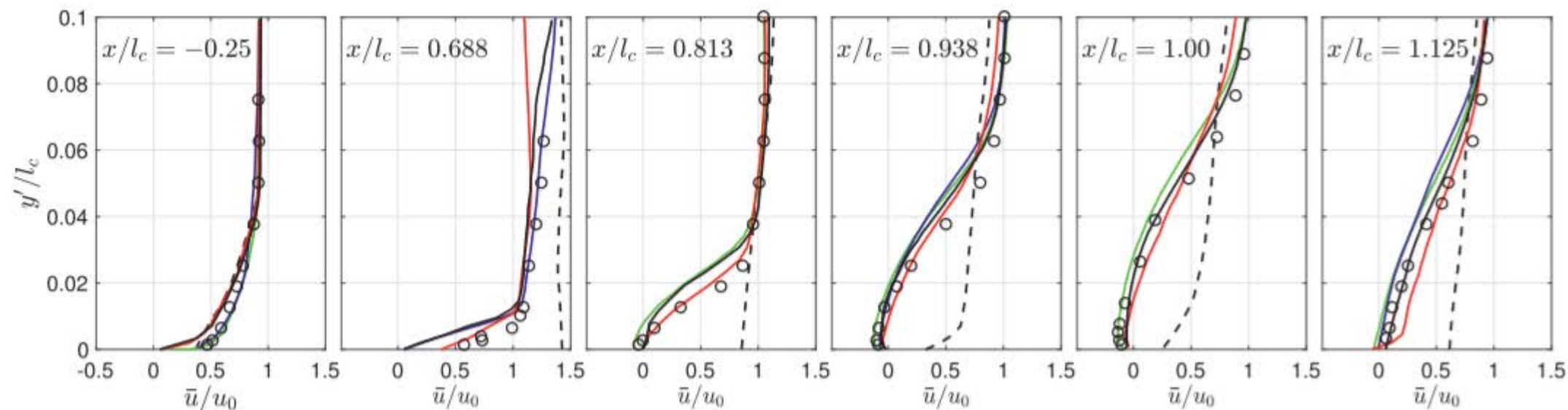
- LES results: pressure coefficient





WMLES of NASA transonic bump configuration

- LES results: time-averaged streamwise velocity



— Present WMLES results

○ Bachalo & Johnson (1986), exp. data,

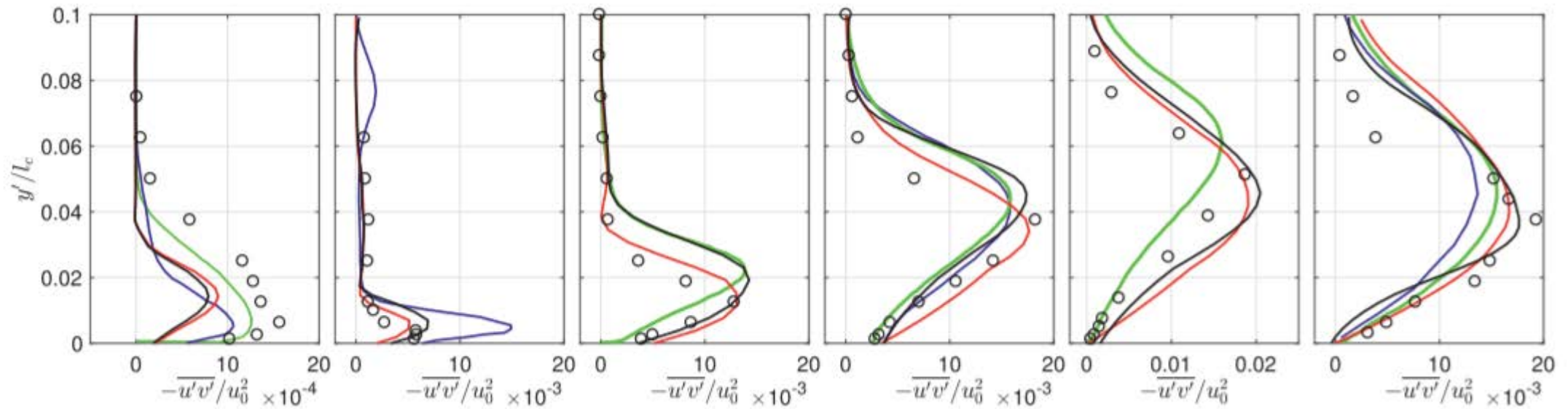
— Spalart et al. (2017), DES+DNS, 8.5B pts

— Uzun & Malik (2018), wall-resolved LES, 24B pts



WMLES of NASA transonic bump configuration

- LES results: Reynold stress



— Present WMLES results

— Spalart et al. (2017), DES+DNS, 8.5B pts

○ Bachalo & Johnson (1986), exp. data,

— Uzun & Malik (2018), wall-resolved LES, 24B pts