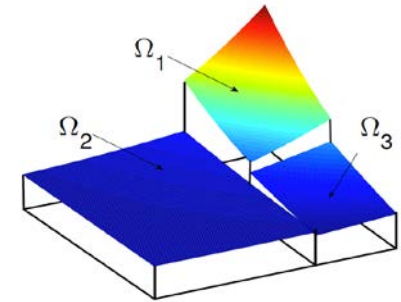




# Introduction to high-order DG method

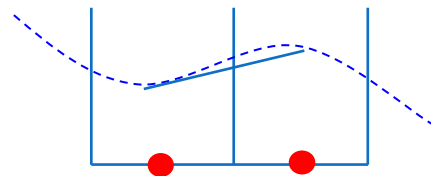
Governing equations:

$$\frac{\partial U}{\partial t} + \nabla \cdot \mathbf{F} = \nabla \cdot \mathbf{Q}$$



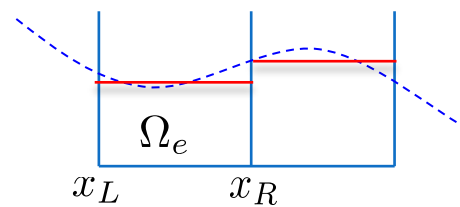
FD

$$\frac{(F_{i+1} - F_i)}{\Delta x}$$



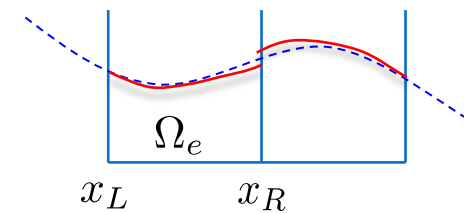
FV

$$\begin{aligned} \int_{\Omega_e} \partial_x F dx \\ = F(x_R) - F(x_L) \\ \approx \hat{F}(x_R) - \hat{F}(x_L) \end{aligned}$$



DG

$$\begin{aligned} \int_{\Omega_e} \phi \partial_x F dx \\ = (\phi F)|_{x_L}^{x_R} - \int_{\Omega_e} F \partial_x \phi dx \\ \approx (\phi \hat{F})|_{x_L}^{x_R} - \int_{\Omega_e} F \partial_x \phi dx \end{aligned}$$





# Introduction to high-order DG method

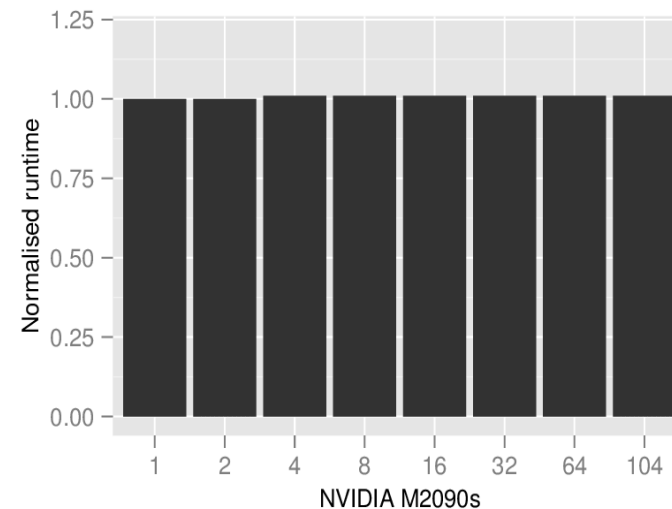
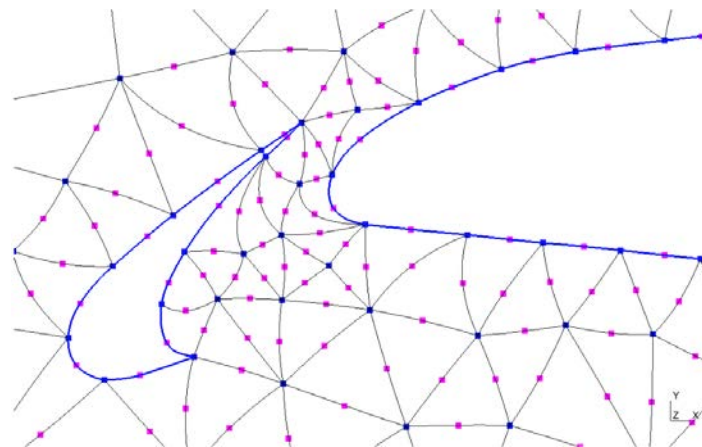
## Advantages:

- Compactness
- Superconvergence
- Energy stability
- Adaptivity
- Real-world geometry
- Data locality for HPC

## Discontinuous schemes:

- discontinuous Galerkin (Reed & Hill, 1973)
- flux reconstruction (Huynh, 2007)
- discontinuous spectral element (Kopriva, 2002)
- spectral difference (ZJ Wang, 2006)

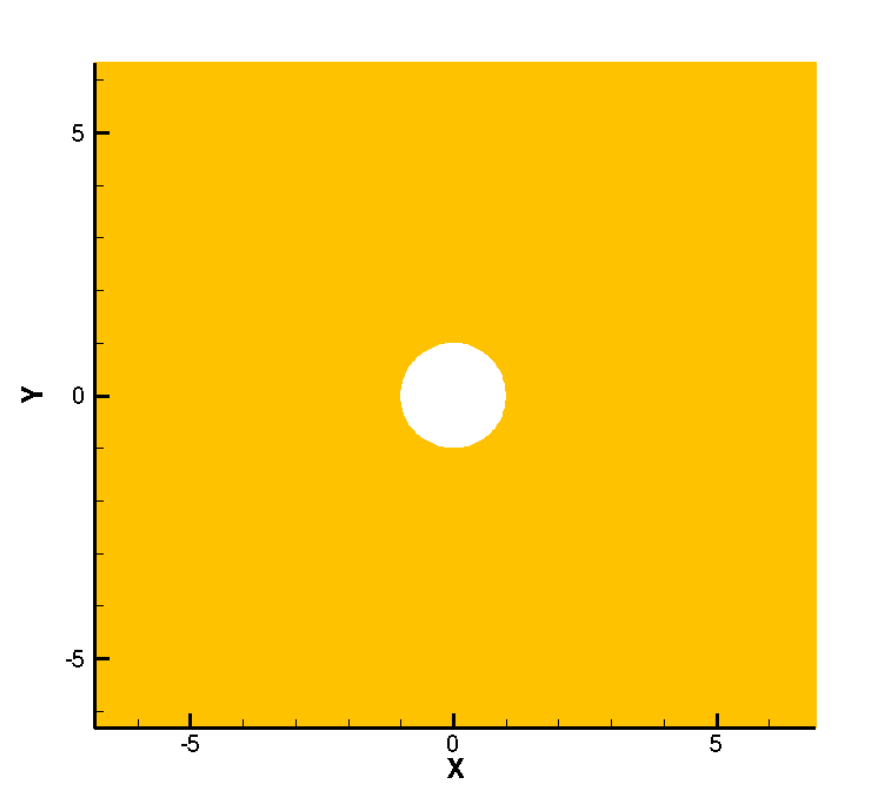
...





# Robustness issue of high-order DG scheme

Illustration of the robustness issue in DG:



DGP4 solution of Mach 0.38 inviscid flow over cylinder

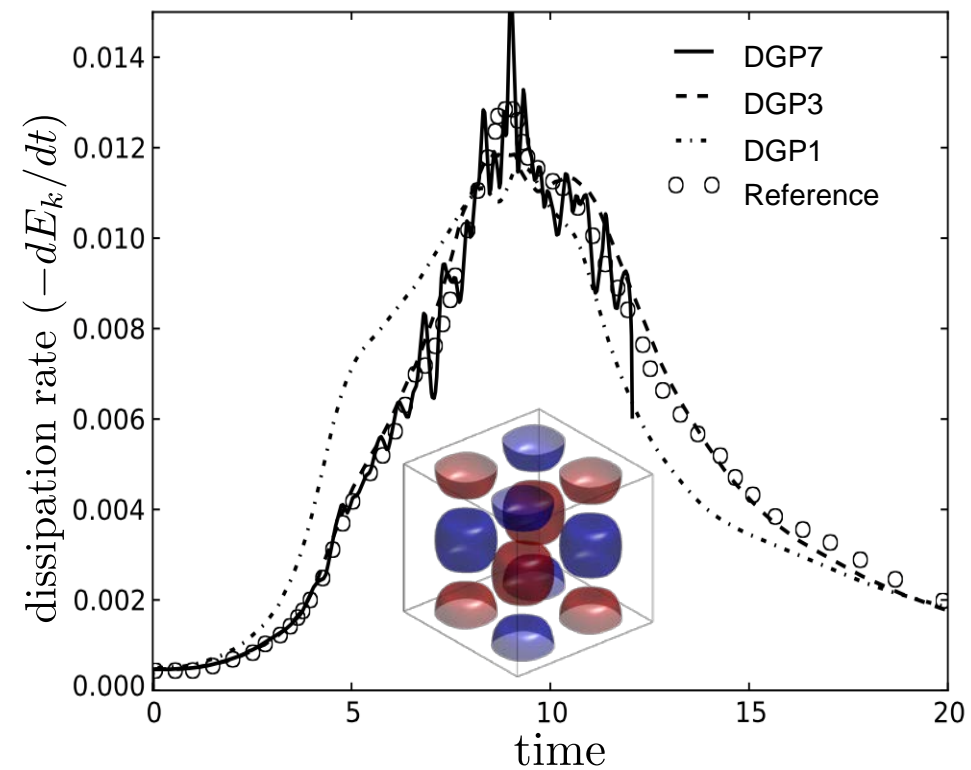


Figure credits: first high-order workshop, 2012.  
Bull & Jameson, *AIAA J.*, 2015.



# Need of a robust and high-order scheme

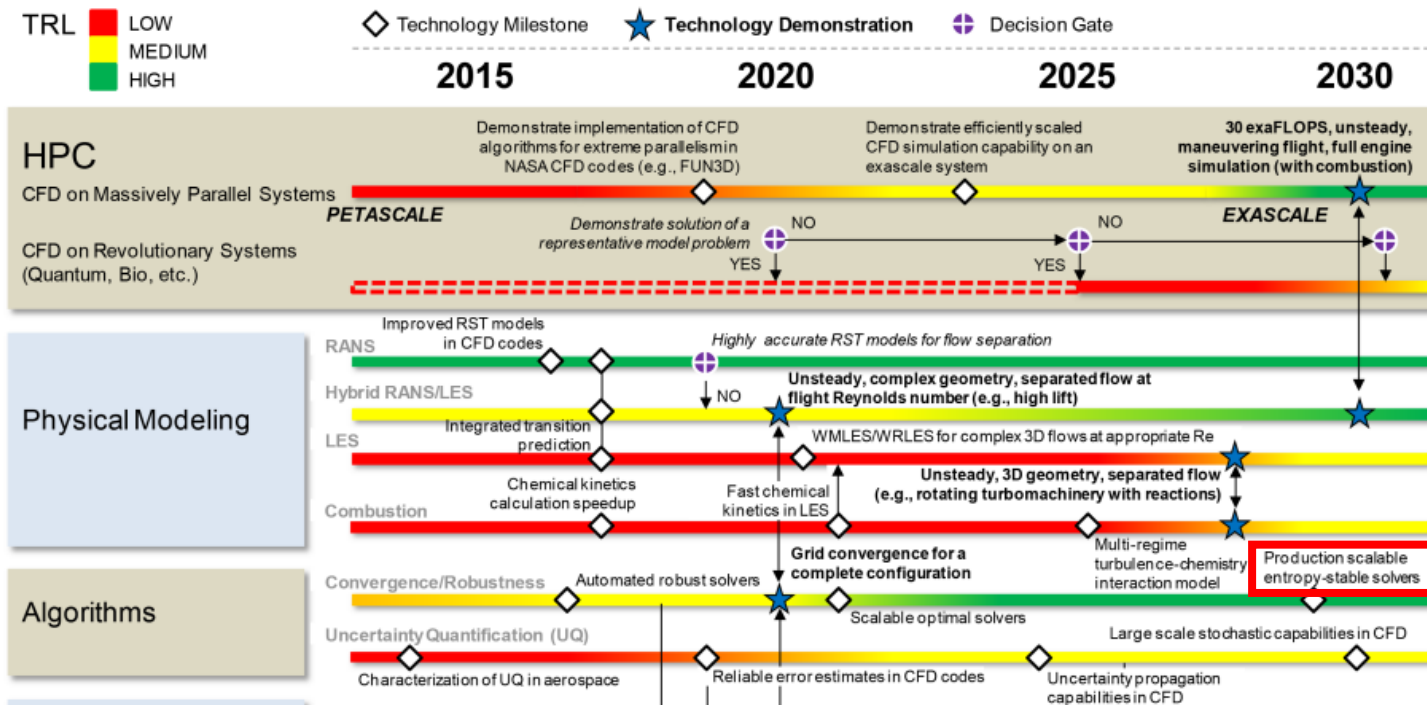
National Aeronautics and Space Administration



## CFD Vision 2030 Study: A Path to Revolutionary Computational Aerosciences

“Longer term, high-risk research should focus on the development of truly enabling technologies such as monotone or *entropy stable schemes* in combination with innovative solvers...”

“Toward the 2030 time frame, it is anticipated that novel *entropy stable formulations* will begin to bear fruit for industrial simulations”





# Entropy-bounded DG scheme

- Governing equations:

$$\partial_t \mathbf{U} + \nabla \cdot \mathbf{F} = 0$$

$$\mathbf{U} = [\rho, \rho u, \rho E, \rho Y]^T$$

$$\mathbf{F} = [\rho u, \rho u^T u + p \mathbf{I}, u(\rho E + p), \rho u Y]^T$$

- Entropy function:

$$s = \log(p/\rho^\gamma), \quad \text{quasi-concave function of } \mathbf{U}$$

- Physical principles:

1.  $p > 0$ , concave function of  $\mathbf{U}$
2.  $\rho > 0$ , convex/concave function of  $\mathbf{U}$
3.  $s \geq s_0$ ,  $s_0$  is the minimum entropy on a domain  $\Omega$  over a finite time interval  $[0, \Delta t]$  (the 2<sup>nd</sup> law of thermodynamics)
4.  $Y \in [0, 1]$



# Entropy-bounded DG scheme

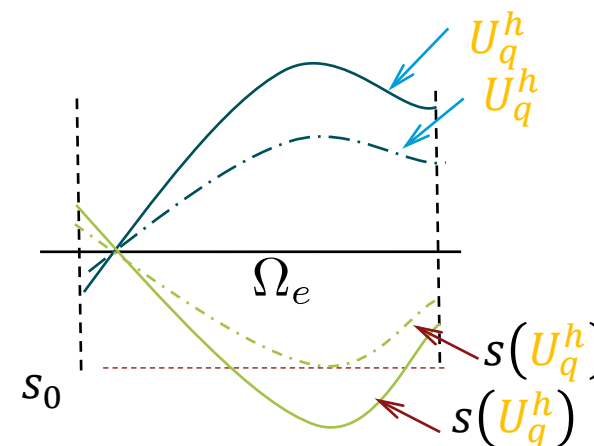
## Key idea:

- Impose the inequality physical principles on discrete solutions to ensure “**physical realizability**”

$$\begin{cases} \rho(U_q^h) \geq 0 \\ p(U_q^h) \geq 0 \\ s(U_q^h) \geq s_0 \end{cases}$$

## Key algorithmic ingredients:

1. Limiters to enforce  $s(U_q^h) \geq s_0$
2. Sufficient condition to guarantee  $s(\bar{U}_e^h) \geq s_0$





# Entropy-bounded DG scheme


Limiter:

- Linear-scaling of elementwise local solutions
- Exploit Jensen's inequality based on convexity/concavity

Define  ${}^L U_e = U_e + \epsilon(\bar{U}_e - U_e)$  and given  $s(\bar{U}_e) \geq s_0$ , find the smallest  $\epsilon$ , such that  $\forall x_q$ ,

1.  $\rho({}^L U_e(x_q)) > 0$
2.  $s({}^L U_e(x_q)) \geq s_0$

Apply Jensen's inequalities to expand (1) and (2):

1.  $(1 - \epsilon)\rho(U_e(x_q)) + \epsilon\rho(\bar{U}_e(x_q)) > 0$
2.  $p({}^L U_e(x_q)) \geq \exp(s_0)\rho^\gamma({}^L U_e(x_q))$  

$$(1 - \epsilon)p(U_e(x_q)) + \epsilon p(\bar{U}_e(x_q)) \geq \exp(s_0) \left[ (1 - \epsilon)\rho^\gamma(U_e(x_q)) + \epsilon\rho^\gamma(\bar{U}_e(x_q)) \right]$$

Note:  $s_0 \rightarrow -\infty$ , this becomes PP limiter



# Entropy-bounded DG scheme

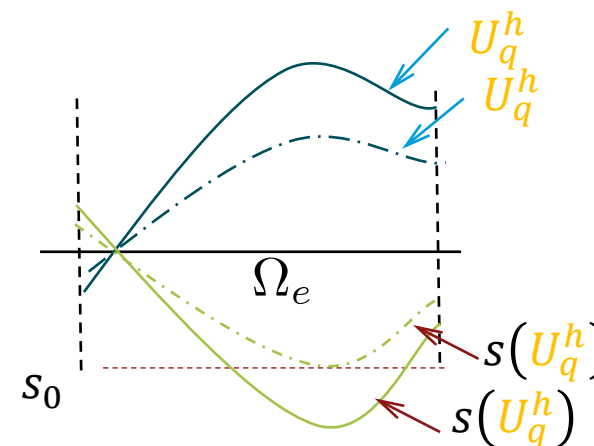
## Key idea:

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# Entropy-bounded DG scheme

The cell-average of DG solution after one time-step

$$\bar{U}_e^{t+\Delta t} = \sum_q \bar{w}_q U_e(x_q, t+\Delta t) = \sum_q \bar{w}_q \left( \hat{F}(U_e(x_l), U_{e-1}(x_l), -\vec{n}) + \hat{F}(U_e(x_r), U_{e+1}(x_r), \vec{n}) \right) \frac{\Delta t}{h}$$

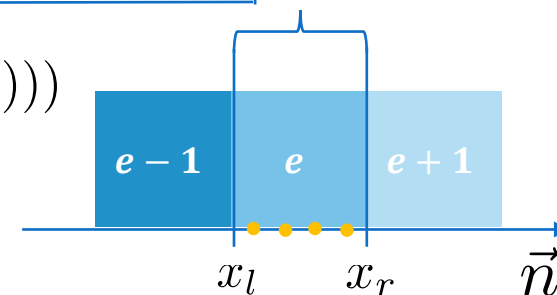
$$= \sum_q (w_q - \beta_l \phi_q(x_l) - \beta_r \phi_q(x_r)) U_e(x_q) \quad \leftarrow \quad U_e(x_{l,r}) = \sum_q \phi_q(x_{l,r}) U_e(x_q)$$

$$+ \beta_l U_e(x_l) - \frac{\Delta t}{h} \left( \hat{F}(U_e(x_l), U_{e-1}(x_l), -\vec{n}) + \hat{F}(U_e(x_l), U_e^*, \vec{n}) \right)$$

$$+ \beta_r U_e(x_r) - \frac{\Delta t}{h} \left( \hat{F}(U_e(x_r), U_e^*, -\vec{n}) + \hat{F}(U_e(x_r), U_{e+1}(x_r), \vec{n}) \right)$$

new CFL numbers  
 $\frac{\beta_l \Delta t}{h}$     $\frac{\beta_r \Delta t}{h}$

$$U_e^* = \frac{1}{2} (U_e(x_l) + U_e(x_r)) - \frac{1}{2\lambda} (F(U_e(x_r)) - F(U_e(x_l)))$$



This is a solution of **Lax Scheme**

(P. D. Lax. Contributions to Nonlinear Functional Analysis, pages 579 603–634. Academic Press, New York, London, 1971.)





## Three-point FVM system:

- The temporally-updated first-order solution written as

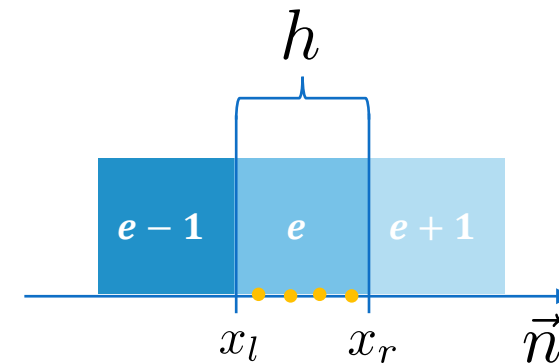
$$\tilde{U}_e^{t+\Delta t} = \tilde{U}_e - \frac{\Delta t}{h} \left( \hat{F}(\tilde{U}_e, \tilde{U}_{e-1}, -\vec{n}) + \hat{F}(\tilde{U}_e, \tilde{U}_{e+1}, \vec{n}) \right)$$

**Lemma:**  $s(\tilde{U}_e^{t+\Delta t}) \geq \min_{k \in \{e, e \pm 1\}} (s(\tilde{U}_k)) = s_0$

- if  $\hat{F}(U_+, U_-, \vec{n})$  is an entropy-stable flux (e.g., LF flux)
- CFL condition  $\Delta t \lambda / h \leq \alpha$

## Proof:

- 1D version: E. Tadmor, *Appl. Numer. Math.*, 1986
- 3D version: Y. Lv & M. Ihme, *J. Comput. Phys.*, 2015





# Entropy-bounded DG scheme

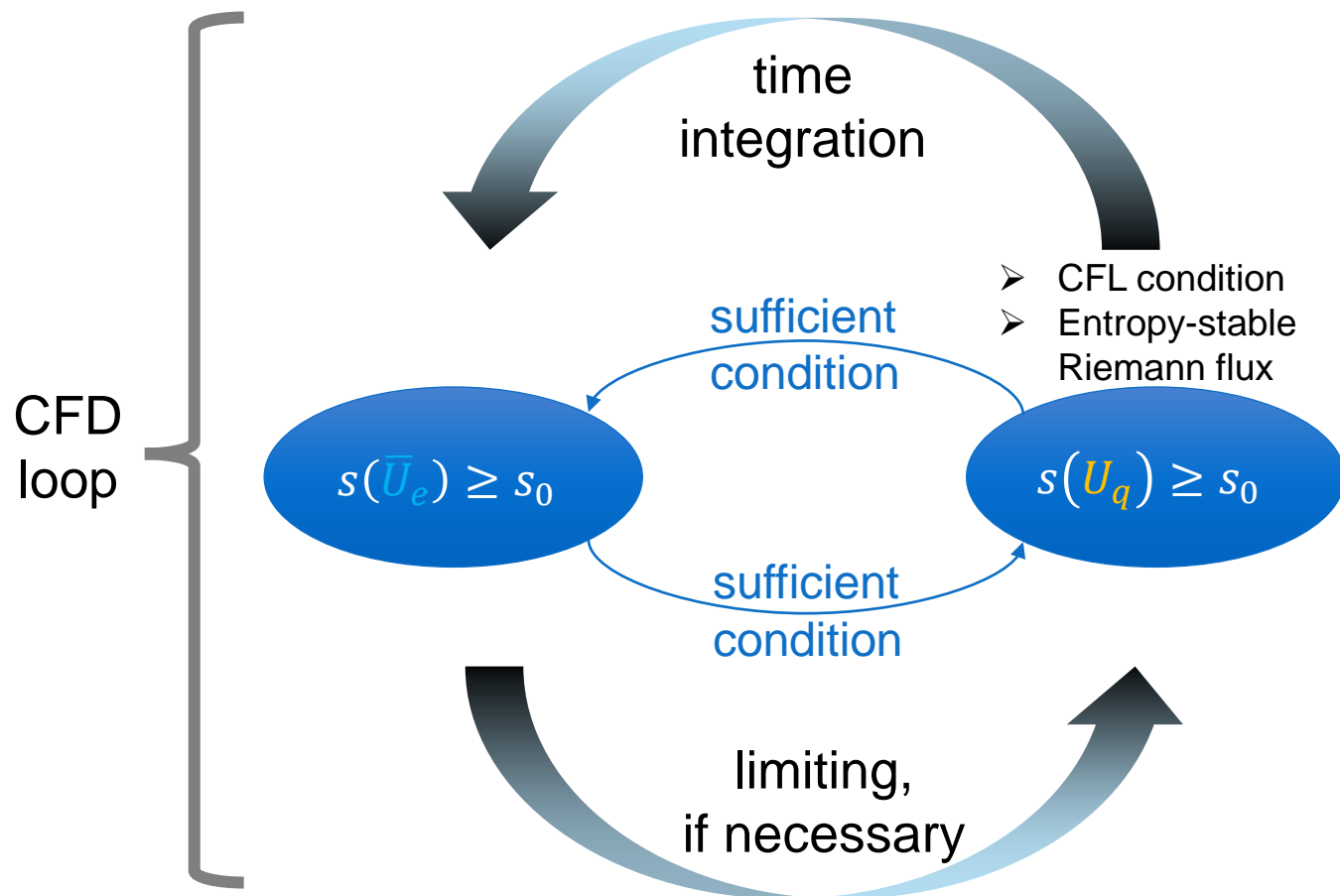
- CFL obtained for different element shapes

Element	Order	QR on $\partial\Omega_e$	QR on $\Omega_e$	CFL <sup>EB</sup>	Element	Order	QR on $\partial\Omega_e$	QR on $\Omega_e$	CFL <sup>EB</sup>
	$p = 1$	/	3	0.5		$p = 1$	3	3	0.167
	$p = 2$	/	5	0.167		$p = 2$	5	5	0.056
	$p = 3$	/	7	0.123		$p = 3$	7	7	0.041
	$p = 4$	/	9	0.073		$p = 4$	9	9	0.024
	$p = 1$	3	3	0.25		$p = 1$	4	3	0.066
	$p = 2$	5	5	0.083		$p = 2$	5	5	0.035
	$p = 3$	7	7	0.062		$p = 3$	8	7	0.015
	$p = 4$	9	9	0.036		$p = 4$	9	9	0.013
	$p = 1$	3	4	0.135	<p>Note: Quadrature rule (QR) applied: Line, Quadrilateral and Brick: tensor-product Gauss-Legendre; Triangle: Dunavant; Tetrahedron: Zhang, et al.</p>				
	$p = 2$	5	5	0.067					
	$p = 3$	7	8	0.058					
	$p = 4$	9	9	0.033					

- CFL number can be found for high-order curved elements, which will be element-specific.



# Entropy-bounded DG scheme

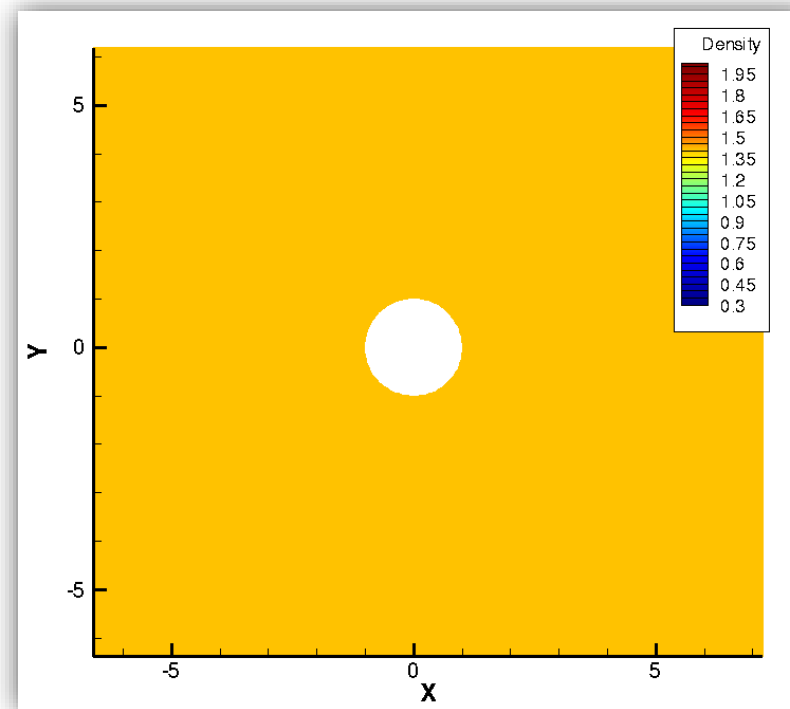
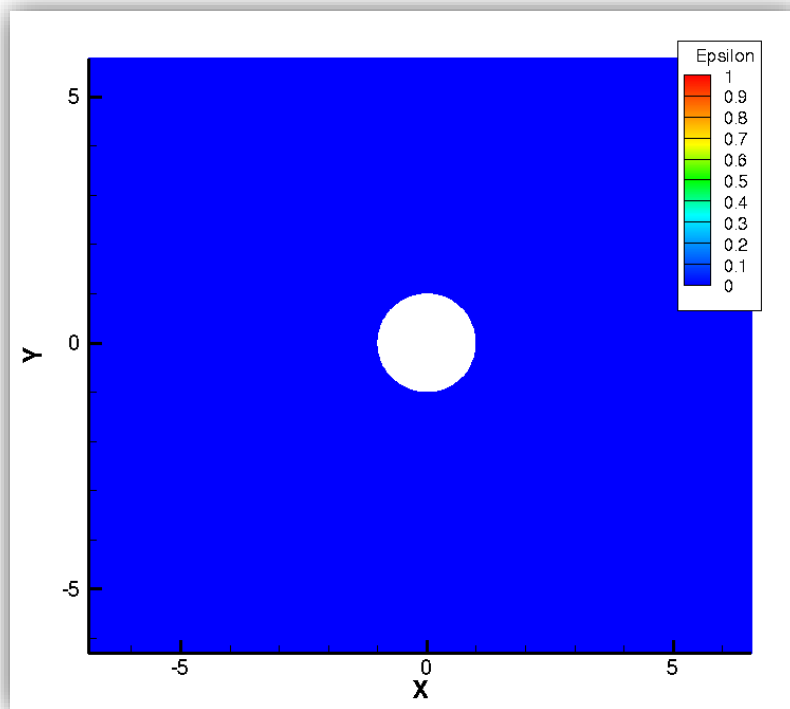




# Entropy-bounded DG scheme

Finding 1:

EBDG prevents non-physical solutions during transient stages





# Entropy-bounded DG scheme

Finding 2:

**EBDG preserves the optimal convergence for smooth solutions**

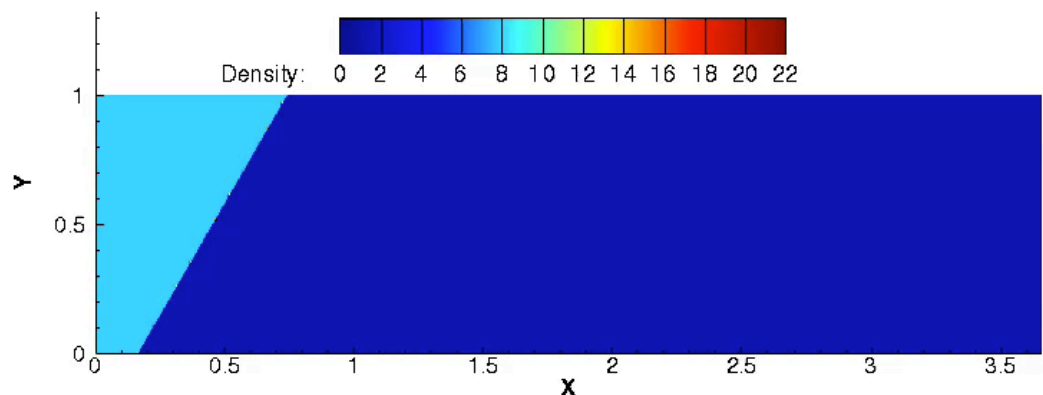
Mesh	DGP1		DGP2		DGP3	
	$L_2$ -error	rate	$L_2$ -error	rate	$L_2$ -error	rate
Quadrilateral Elements						
Level 1	7.272e-2	-	1.694e-2	-	3.816e-3	-
Level 2	1.318e-2	2.464	7.219e-4	4.552	1.827e-4	4.384
Level 3	2.441e-3	2.433	6.029e-5	3.582	1.036e-5	4.141
Triangular Elements						
Level 1	1.137e-1	-	2.590e-2	-	4.086e-3	-
Level 2	1.865e-2	2.608	8.899e-4	4.863	1.291e-4	4.984
Level 3	3.391e-3	2.459	7.222e-5	3.623	6.939e-6	4.217



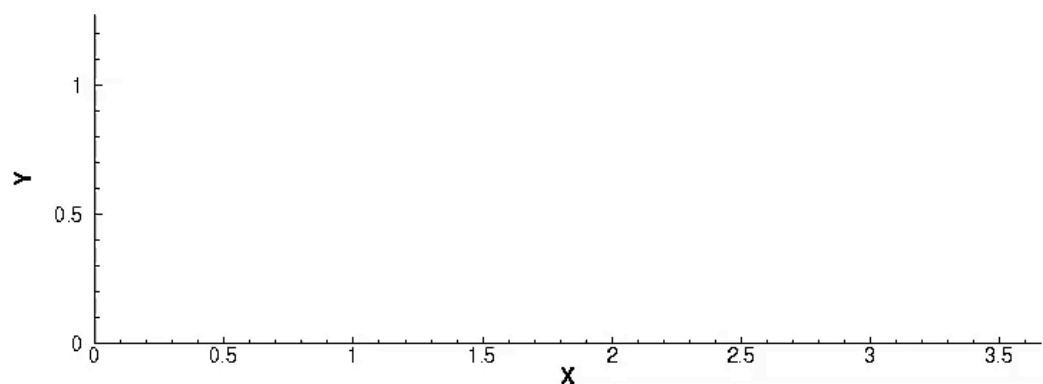
# Entropy-bounded DG scheme

Finding 3:

**EBDG ensures nonlinear stability for arbitrary flow conditions and/or mesh configurations**



◀ Solution



◀ Trouble-cell marker